

# 3 ournal of Engineering and Sustainable Development

Vol. 23, No.04, July 2019 ISSN 2520-0917 https://doi.org/10.31272/jeasd.23.4.3

# AN EFFICIENET ALGORITHM FOR STATIC STATE ESTIMATION IN ELECTRIC POWER SYSTEM

Mohammed Falih Hasan<sup>1</sup>, \*Dr. Kassim Abdulrezak Al-Anbarri<sup>2</sup>

1) Msc.Student Electrical Engineering Department, Mustansiriyah University, Baghdad, Iraq.

2) Assistant Prof., Electrical Engineering Department, Mustansiriyah University, Baghdad, Iraq.

Received 4/12/2017 Accepted 23/4/ 2018 Published 1/7/2019

**Abstract:** This paper presents an efficient static state estimator that is suitable for real time monitoring of the power system. The proposed algorithm includes a weighted least square (WLS) method based on rectangular coordinates system. A predictor-corrector iterative technique is used in solving the state estimator model which is described by a set of nonlinear equations relating measured quantities and the state variables. The proposed algorithm is enhanced by selecting the allocation the PMUs meters optimally by using Particle Swarm Optimization (PSO). The proposed algorithm is applied to the IEEE-14 bus and IEEE-30 bus test systems. The obtained results reveal the significant contribution of the proposed algorithm in optimal estimate of the static state in terms of number of iterations for convergence, execution time and accuracy.

Keywords: State estimation, rectangular coordinates, Phasor measurement units, predictor-corrector.

# خوارزمية كفوءة لتخمين الحالة الساكنة في منظومة القدرة الكهربائية

الخلاصة. يقدم هذا البحث خوارزمية جديدة كفوءة لتخمين الحالة الساكنة لمنظومة القدرة ملائمة للمراقبة الزمنية الحقيقية. تتضمن الخوارزمية المقترحة طريقة العامل التربيعي الاصغر الموزون بالاستناد على استخدام الاحداثيات المتعامدة لمتغيرات الحالة. تم استخدام تقنية التنبؤ والتصويب العددية في حل نموذج مخمّن الحالة الموصوف بمجموعة من المعادلات غير الخطية التي تربط الكميات المقاسة و متغيرات الحالة. تم تعزيز الخوارزمية باختيار المواقع المثلى لاجهزة قياس زاوية الطور باستخدام طريقة تقنية أمثلية الحشرات المقاسة و تم تطبيق الخوارزمية المقترحة على منظومة معهد المهندسين الكهربائيين القياسية ذات (14) عقدة و (30) عقدة. وقد أظهرت النتائج المستحصلة المساهمة المهمة للخوارزمية المقترحة في التخمين الامثل للحالة الساكنة لمنظومة القدرة بدلالة عدد التي ت لاقتراب الحل، زمن التنفيذ والدقة.

# 1. Introduction

Static state estimation is an essential analysis utilized in the real-time monitoring of the power system. It is the cornerstone of the power system security analysis. State estimation determines the optimal static state of the system (voltage magnitude and phase angle) by processing the available measurements based on an appropriate system model. Extensive research have been carried out which addressed the various functions

<sup>\*</sup>Corresponding Author alanbarri@uomustansiriyah.edu.iq

of the state estimation since the first attempt made by Schweppe [1,2]. Different approaches have been proposed covering network topology processing [3-10].

The improvement of the state estimator by maintaining system observability has been demonstrated in [11-14]. Several techniques have been introduced on bad data detection and elimination [15-19]. Optimal estimate of the state vector is attracting the attention of many researchers. The most commonly used method in obtaining the optimal solution vector is the weighted least square (WLS). The state estimator model is described by a set of nonlinear equations relating measured quantities and the state variables. Singh and Alvarado proposed a weighted least absolute value state estimator by using interior point methods [20]. An attempt to obtain the optimum state vector based on singular value decomposition was proposed by Madtharad [21]. State estimation by using bilinear approach by introducing auxiliary state variables and auxiliary measurements were presented in [22, 23]. A state estimator algorithm based on fast decoupled WLS was presented in [24]. Abbasi and Seifi [25] suggested a master-slave-splitting technique to estimate the state variables of global power system. State estimator algorithm using a direct non-iterative method was given in [26]. A probabilistic approach to power system state estimation was demonstrated in [27]. A regularized based state estimator was developed in [28] to overcome the numerical instability of ill-conditioned state estimation problems. Recently, it was found that the redundancy in measurements can be achieved by incorporating the phasor measurements unit (PMU) in power system monitoring [29-31]. Since the solution of a WLS state estimator is based on iterative technique, it is very important to develop an algorithm that determines the optimal state accurately in a short time and suitable for real time application.

In this paper an efficient algorithm is proposed to obtain the optimal static state vector by using the WLS based on the rectangular coordinates of the state vector. The proposed algorithm deployed a predictor-corrector numerical technique in determining the state vector. The proposed algorithm is integrated with another algorithm that identifies the optimal placement of PMU meters and conventional meters by using an artificial technique, namely Particle Swarm Optimization technique.

This paper is organized as follows: Section 2 reviews the traditional weighted least square method. The state estimator model based on rectangular coordinate is presented in section 3. Section 4 presents the elements of the proposed algorithm. In Section 5, a discussion of the results obtained by applying the proposed algorithm on typical test systems is presented. Finally, section 6 presents the conclusion.

#### 2. Traditional WLS Technique

The vector of measured quantities is related to the state vector by the following nonlinear system of equation [32]:

$$[z] = [h_{(x)}] + [e] \tag{1}$$

where:

#### [z]: Measurement vector

 $[h_i(x)]$ : nonlinear function describes the  $i^{th}$  measurement in terms of the state variables

x : system state vector (voltage magnitudes and angles)

 $[e_i]$ : the error of the  $i^{th}$  measurement

The best solution of state estimate vector x may be determined by minimizing the sum of weighted squares of residuals

$$\min J(\hat{x}) = \sum_{i=1}^{m} \frac{e_i^2}{\sigma_i^2}$$
(2)

where:

$$[w_i] = [R_i]^{-1} = \left[\frac{1}{\sigma_i^2}\right]$$

 $[R_i]$ : is a diagonal matrix whose elements are the variances of the measurement error.  $[w_i]$ : weighting factor is defined by the inverse of the measurements variances. Consequently, measurements of a higher quality have smaller variances that relates to their weights. Equation (2) can be represented in matrix form:

$$\min J(\hat{x}) = [z - h(\hat{x})]^T R^{-1} [z - h(\hat{x})]$$
(3)

The necessary conditions for a minimum is that :

$$g(x) = \frac{\partial J(x)}{\partial x} = -H(x)^T R^{-1} [z - h(x)] = 0$$
(4)

Where, 
$$[\mathbf{H}(x)] = \left[\frac{\partial \mathbf{h}(x)}{\partial x}\right]$$
  
$$x^{k+1} = x^{k} - \left[G(x^{k})\right]^{-1} g(x^{k})$$
(5)

$$G(x^{k}) = \frac{\partial g(x^{k})}{\partial x} = \left[H(x^{k})\right]^{T} R^{-1}[z - h(x^{k})]$$
<sup>(6)</sup>

$$G(x^k) = \left[ \mathrm{H}(x^k) \right]^T R^{-1} \left[ \mathrm{H}(x^k) \right]$$
<sup>(7)</sup>

$$[G(x^k)][\Delta x^{k+1}] = [F(x_i)] \tag{8}$$

Where,

 $[F(x_i)] = [H(x^k)]^T R^{-1} [z - h(x^k)]$   $\Delta x^{k+1}: deviation of state factor = x^{k+1} - x^k$   $[H(x)] is the measurement Jacobian matrix of dimension (m \times n)$  k: iteration index  $x^k: is the state vector at iteration k$ [G(x)]: the gain matrix Equation(8) is solved iteratively for the state vector until Max  $|\Delta x^k| < \varepsilon$  where  $\varepsilon$  is a very small value.

#### 3. Formulation of the State Estimator by using Rectangular Coordinates

The rectangular coordinate system has a better conditioning of a WLS estimation process than for the polar coordinate system. Since the polar coordinate is represented by transcendental functions, the Taylor series expansion of these functions is an infinite one. The rectangular coordinate system is based on quadratic terms. This leads to a major simplification of an expansion in Taylor series for J(x) in the rectangular coordinate is described by the following rectangular form:

$$V_i = e_i + jf_i \tag{9}$$

where,  $e_i$ ,  $f_i$ : a real and imaginary part of the voltage at bus *i* respectively The state vector of the system is described as $[\mathbf{x}]^T = [f_2 f_3 \dots f_n e_1 e_2 \dots e_n]$ The real and reactive power injection at bus *i*:

$$P_{i} = \sum_{j=1}^{N} \left( e_{i}e_{j}G_{ij} - e_{i}f_{j}B_{ij} + e_{j}f_{i}B_{ij} + f_{i}f_{j}G_{ij} \right)$$
(10)

$$Q_i = \sum_{j=1}^{N} \left( -e_i e_j B_{ij} - e_i f_j G_{ij} + e_j f_i G_{ij} - f_i f_j B_{ij} \right)$$
(11)

The real and reactive power flow from bus *i* to bus *j* :

$$P_{ij} = -e_i^2 G_{ij} + e_i e_j G_{ij} - e_i f_j B_{ij} - f_i^2 G_{ij} + e_j f_i B_{ij} + f_i f_j G_{ij}$$
(12)

$$Q_{ij} = e_i^2 B_{ij} - e_i e_j B_{ij} - e_i f_j G_{ij} + f_i^2 B_{ij} + e_j f_i G_{ij} - f_i f_j B_{ij}$$
(13)

The structure of the measurement Jacobian [H] will be as follows :

$$[H] = \begin{bmatrix} \frac{\partial V}{\partial f} & \frac{\partial V}{\partial e} \\ \frac{\partial P_i}{\partial f} & \frac{\partial P_i}{\partial e} \\ \frac{\partial Q_i}{\partial f} & \frac{\partial Q_i}{\partial e} \\ \frac{\partial P_{ij}}{\partial f} & \frac{\partial P_{ij}}{\partial e} \\ \frac{\partial Q_{ij}}{\partial f} & \frac{\partial Q_{ij}}{\partial e} \end{bmatrix}$$

#### 4. Proposed Algorithm

In the initial phase of the proposed algorithm, the PMU devices to be installed have to be placed optimally by using Particle Swarm Optimization technique. This optimal location will maintain a redundancy in the measurements and improve the observability of the system.

#### 4.1 Augmentation of the PMU in the Estimator Model

Let  $[z_2]$  indicate PMU measurements, which contain voltage magnitudes, voltage angles, real and imaginary parts of current phasors. The matrix  $[R_2]$  represents the measurement error covariance matrix of  $[z_2]$ . By adding the vector of PMU measurements  $[z_2]$  to the vector of conventional measurement  $[z_1]$  yields The new measurement set [z].

$$[z] = \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} = \begin{bmatrix} z_1 \\ v_{PMU\_mag} \\ v_{PMU\_ang} \\ I_{PMU\_real} \\ I_{PMU\_Img} \end{bmatrix}$$
(14)

where,  $V_{PMU_mag}$  is the voltage magnitude measured by PMUs and  $V_{PMU_ang}$  is the phase angle measured by PMUs.  $I_{PMU_real}$  and  $I_{PMU_lmg}$  are the real part and imaginary part of the current measured by PMUs.

Current phasor measurements can be included in the SE model by using the rectangular representation:

$$I_{PMU\_real} = e_i G_{ij} - e_j G_{ij} - f_i B_{ij} + f_j B_{ij} - \frac{B}{2} f_i$$
(15)

$$I_{PMU\_Img} = f_i G_{ij} - f_j G_{ij} + e_i B_{ij} - e_j B_{ij} + \frac{B}{2} e_i$$
(16)

Let [h(x)] and  $[h_2(x)]$  be the nonlinear equations of new measurement set [z] and PMU measurements $[z_2]$ , respectively. The new Jacobian matrix corresponding to the measurement set [z] will be given as follows:

$$[H] = \begin{bmatrix} H_1 \\ H_2 \end{bmatrix} = \begin{bmatrix} \frac{\partial h_1(x)}{\partial x} \\ \frac{\partial h_2(x)}{\partial x} \end{bmatrix}$$
(17)

Therefore, the state solution of the WLS state estimator can be written as follows:

$$[x_{i+1}] = [x_i] + [H^T R^{-1} H]^{-1} [H]^T [R]^{-1} [z - h(x_i)]$$
(18)

where, the error covariance matrix of measurement set[z] with mixing is

$$[R] = \begin{bmatrix} R_1 & 0\\ 0 & R_2 \end{bmatrix}$$
(19)

#### 4.2 Particle Swarm Optimization(PSO)

Eberhart and Kennedy presented a Particle swarm optimization (PSO) in 1995 as a good substitute to genetic algorithm (GA). PSO is one of the population based artificial intelligence (AI) algorithms. PSO concept was used to graphically simulate the smart and unforeseeable choreography of a bird flock, with the aim of detecting patterns that govern the ability to fly synchronously, and to suddenly alternate direction with a regrouping in an optimal formation. With this in consideration, it was realized that the conceptual model was, indeed a simple and efficient optimization algorithm. Each particle(individual) in the population can be considered as candidate solution. The location of each particle is symbolized by xy-axis site. The symbol  $v_x$  (the velocity of x-axis) represents velocity (displacement vector) while  $v_y$  represents (the velocity of y-axis). The location and the velocity information of the individual are used in modifying the location of the individual[34].

This modification can be expressed by the concept of velocity. The velocity of each individual is adjusted by the following equation:

$$v_i^{k+1} = w_i \ v_i^{k} + c_1 \ rand_1 \times (Pbest_i - s_i^{k}) + c_2 \ rand_2 \times (gbest_i - s_i^{k})$$
(20)

where  $v_i^k$  is present velocity of individual *i* at iteration *k*,  $rand_1$  and  $rand_2$  are random numbers between 0 and 1,  $s_i^k$  is present site of individual *i* at iteration *k*, *Pbest<sub>i</sub>* is *Pbest* of individual *i*, *gbest* is *gbest* of the group,  $w_i$  is weight function for speed of individual *i*, generally, the variation of the value of  $w_i$  is assumed to be linear from 0.9 to 0.4 as the iterative process continues.  $c_i$  is weight constants for cognitive and neighboring term.

Typically, the weighting function is used in following equation (20):

$$w = w_{max} - \frac{w_{max} - w_{min}}{iter_{max}} \times iter$$
(21)

where  $w_{max}$  is the initial weight,  $w_{min}$  is final weight, *iter<sub>max</sub>* is maximum iteration number, *iter* is iteration index. Using the above equation (21), diversification characteristics is progressively reduced. Based on equation (20), a specific velocity that progressively obtains close to pbests and gbest can be calculated. The present site (searching point in the solution space) can be adjusted by the following formula:

$$s_i^{k+1} = s_i^k + v_i^{k+1} \tag{22}$$

#### 4.3 Optimal Placement Algorithm of PMU

**Step1**: Inputting traditional SCADA measurements which include bus voltages, line flows and power injections. Also inputting PMUs Measurements which include voltage magnitude, angle, real and imaginary parts of current. Inputting bus limit.

**Step2**: Initializing the PSO parameters. Setting up the set of PSO parameters such as, number of individuals (Number of variables (N)), acceleration constants (C1 and C2), maximum number of iteration, maximum and minimum of Inertia weight (W) and Population size.

Step3: Calculating the state estimation by using the traditional method (WLS).

**Step4**: Randomly creating an initial population of individuals (locations of PMU) ,and the positions and the velocities of the individuals. Setting the iteration counter = 0.

**Step5**: For each individual (location of PMU), if the bus number is within the limits, the state estimation is calculated using WLS method. Otherwise, that individual (location of PMU) is not feasible.

**Step6**: Recording and updating the best values. The two best values are stored in the searching process. Each individual moves in the direction related to its previously best solution it has reached so far which is stored as  $P_{best}$ . Another best value to be stored is the  $G_{best}$ , which accounts for the global best value achieved by neighboring individuals.  $P_{best}$  and  $G_{best}$  are the minimum value of the objective function. This step also updates  $P_{best}$  and  $G_{best}$ . Initially, the fitness of each individual is compared with its  $P_{best}$ . If the current solution is better than its  $P_{best}$ , then  $P_{best}$  is replaced by the current solution. Then, the fitness of any particle is compared with  $G_{best}$ . If the fitness of any individual is better than  $G_{best}$ , is replaced.

**Step7**: Updating the velocity and position of the location of PMU. Equation (20) is applied to update the velocity and position of the individual (location of PMU). A movement in the direction of chosen bus is represented by the velocity of an individual. Meanwhile, the position of the individuals is updated by applying Equation (22).

**Step8**: Checking End criterion. The end criterion is checked, if it is satisfied, the algorithm is stopped; otherwise, step 3-7 is repeated until the end criterion is satisfied. In this work, the individuals are locations of PMUs as shown below:

$$P_{\text{particle}} = \begin{bmatrix} X_1 & X_2 & \cdots & X_n \end{bmatrix}$$
(23)

where,

n: is the number of PMU with selected bus, which limits according to the system size and limitations.

X : location of PMU.

#### **The Constraints**

The PSO procedures must comply with certain constraints: (i) each location of PMU is tested to verify if location number is between 2 and N bus in general (ii) only one PMU can be placed at each bus; (iii) 2 PMU cannot be located at buses at the edges of the same power line. Since PMU also gives information about current phasors in the lines connected to one bus, there is enough information to determine the voltage phasor at the other bus.

#### The Fitness Function (objective function)

In this work, PSO is implemented to find the optimal locations of PMUs through minimizing the following objective function:

$$FF_{min} = [R] - [H][G]^{-1}[H]^{\mathrm{T}}$$
(24)

The process will be continued until the maximum iteration and number of population reaches a prescribed value. Figure (1) shows the procedure of PSO technique. Table (1) illustrates parameters of technique used.



Figure 1. Flowchart of optimal PMUs location

able 1. Parameter of PSO for Optimal Pivios Location
--

For Optimal PMUs Location (Parameter of PSO)	Number or Value
Number of variables (n) (Number of PMUs)	3 PMUs
Maximum Inertia weight (wmax)	0.9
Minimum Inertia weight (wmin)	0.4
Cognitive acceleration factor (C1)	1.5
Social acceleration factor (C2)	1.5
Population size (nPop)	25
Maximum number of iteration(Maxite)	100

## 4.4 Predictor-Corrector Iterative Technique

In a previous paper [35], the author applied successfully a predictor–corrector iterative technique in obtaining load flow solution. A brief description of the predictor –corrector iterative technique is given in Appendix A. The predictor –corrector iterative technique can be applied to equation (8) as follow:

$$[x_{i+1}] = [x_i] + 12 [G_{(x_i)} + 10G_{(w_i)} + G_{(y_i)}]^{-1} [F(x_i)]$$
<sup>(25)</sup>

Where,

 $[G_{(x_i)}]$ : the gain matrix calculated at initial point.

 $[G_{(w_i)}]$ : the gain matrix calculated at mid point.

 $[G_{(y_i)}]$ : the gain matrix calculated at prediction point.

Equation(25) is solved iteratively for the state vector until Max  $|\Delta x^k| < \varepsilon$  where  $\varepsilon$  is a very small value.

#### 5. Results and Discussion

The algorithms are examined and tested on IEEE-14, IEEE-30 bus standard test system. In order to assess the performance of the state estimator, a power flow solution of each system is set as a benchmark for comparison. The Mean Square Error (MSE) is used as index to illustrate the accuracy of the proposed algorithm. MSE is defined in equation (26) as follows:

$$MSE = \frac{1}{N} \sum_{i=1}^{N} (|A_i^{true} - A_i^{est}|^2)$$
(26)

Where, N: number value of measurement.  $A_i^{true}$ : true value of measurement *i*.  $A_i^{est}$ : estimated value of measurement *i*.

#### 5.1 IEEE-14 bus

The proposed algorithm is applied to determine the best estimate vector of IEEE-14 bus test system with a set of 41 conventional meters[36]. An additional three PMU meters have to be installed in the system to improve the observability.

By applying the PSO optimal placement algorithm to the system to select the optimal locations of the PMU meters, it is found that the best location of the meters are buses : 11, 12 and 14. The results of applying the proposed algorithm to the IEEE-14 bus test system are given in Tables (2,3) and Figures (2,3).

There is a clear discrepancy between the true bus bar voltages and the estimated voltages obtained by using traditional WLS, while the estimated voltages vector obtained by using the proposed algorithm is similar to the true voltages. It can be seen that the accuracy of proposed method is better as compared with conventional method (WLS). The MSE for voltage estimates in proposed method (0.000005) is less than WLS (0.00311) as shown from Table (6). Also from Table (7) it can be seen that MSE for bus angle in proposed method (0.0000004) is less than WLS (0.000655).

It is found that the proposed algorithm is converged within 7 iterations, while the traditional WLS algorithm is converged within 13 iterations. On the other hand, the execution time for proposed method less than WLS and that shown in Table (8).

Bus	Voltage	Voltage	Voltage	Abs.	Abs.
No.	Actual	WLS	Proposed	Error	error
	(p.u)	Polar	Algorithm	WLS	Proposed
		Form		Polar	Algorithm
				Form	
1	1.06	1.0068	1.0621	0.0532	0.0021
2	1.045	0.9899	1.0459	0.0551	0.0009
3	1.01	0.9518	1.0093	0.0582	0.0007
4	1.01423	0.9579	1.0145	0.05633	0.00027
5	1.01724	0.9615	1.0179	0.05574	0.00066
6	1.07	1.0185	1.07	0.0515	0
7	1.05034	0.9919	1.0482	0.05844	0.00214
8	1.09	1.0287	1.0826	0.0613	0.0074
9	1.03371	0.9763	1.0335	0.05741	0.00021
10	1.03256	0.9758	1.0325	0.05676	0.00006
11	1.04748	0.9932	1.0474	0.05428	0.00008
12	1.0535	1.0009	1.0534	0.0526	0.0001
13	1.04711	0.9940	1.047	0.05311	0.00011
14	1.02131	0.9647	1.0212	0.05661	0.00011
MSE				0.00311	0.000005
No. of	5	13	7		
iter.					

Table 2.Actual voltages, estimated voltage, and errors for the 14 Bus system



Figure 2. Comparison between actual and estimated values of the bus voltage magnitude

Bus	Angle	Angle	Angle for	Abs.	Abs.
No.	Actual	WLS	Proposed	error	Error for
	(rad.)	(rad.)	Algorithm	WLS	Proposed
			(rad.)		Algorithm
1	0	0	0	0	0
2	-0.08705	-0.09646	-0.08667	0.00941	0.00038
3	-0.2224	-0.2479	-0.22199	0.0255	0.00041
4	-0.17901	-0.19922	-0.17859	0.02021	0.00042
5	-0.15297	-0.17031	-0.15279	0.01734	0.00018
6	-0.25164	-0.28065	-0.2516	0.02901	0.00004
7	-0.23129	-0.25745	-0.23113	0.02616	0.00016

Table 3.Actual volt	age angles, e	stimated and	gles, and erro	ors for the 14	Bus system
		sumaced any	Bies, and en o		Dus system



Figure 3. Comparison between actual and estimated values of the bus phase angle

#### 5.2 IEEE-30 bus System

The set of measurement of the IEEE-30 bus system consists 93 conventional meters [36]. An additional three PMU meters have to be installed in the system to improve the observability. By applying the PSO optimal placement algorithm to the system to select the optimal locations of the PMU meters, it is found that the best locations of the meters are buses: 13, 26 and 30.

From the results of IEEE-30 bus test system in Tables (4,5) and Figures (4,5) reveal that the proposed method is more accurate than the conventional method (WLS). From Table (6) it can be seen that MSE for voltage estimates in proposed method (0.0000068) is less than WLS (0.00553). The MSE for bus angle in proposed method (0.0000017) is less than WLS (0.00185) as shown from Table(7). The number of iteration for proposed method (7 iter.) is less than WLS (12 iter.). On the other hand, the execution time for proposed method is less than WLS and that shown in Table(8).

Table 4.Actual voltages, estimated voltage, and errors for the 30 Bus system

Bus	Voltage	Voltage	Voltage	Abs.	Abs. Error
No.	Actual	WLS polar	Proposed	Error WLS	Proposed
	(p.u)	Form	Algorithm	Polar Form	Algorithm
1	1.06	0.9865	1.0556	0.0735	0.0044
2	1.043	0.97	1.0429	0.073	0.0001
3	1.01964	0.9474	1.0214	0.07224	0.00176
4	1.01041	0.9384	1.013	0.07201	0.00259

5	1.01	0.9335	1.009	0.0765	0.001
6	1.00958	0.9395	1.0143	0.07008	0.00472
7	1.00197	0.9287	1.004	0.07327	0.00203
8	1.01	0.9449	1.0194	0.0651	0.0094
9	1.03925	0.9667	1.04	0.07255	0.00075
10	1.02147	0.9472	1.0224	0.07427	0.00093
11	1.082	1.0093	1.0798	0.0727	0.0022
12	1.04959	0.9746	1.0495	0.07499	0.00009
13	1.071	0.9954	1.0709	0.0756	0.0001
14	1.03202	0.9559	1.0321	0.07612	0.00008
15	1.02508	0.9491	1.0254	0.07598	0.00032
16	1.03042	0.9555	1.0307	0.07492	0.00028
17	1.01876	0.9441	1.0194	0.07466	0.00064
18	1.01145	0.9352	1.012	0.07625	0.00055
19	1.00656	0.9306	1.0073	0.07596	0.00074
20	1.0095	0.9339	1.0102	0.0756	0.0007
21	1.00819	0.9328	1.009	0.07539	0.00081
22	1.01196	0.9372	1.0129	0.07476	0.00094
23	1.00855	0.9331	1.0093	0.07545	0.00075
24	0.99908	0.9231	0.9999	0.07598	0.00082
25	1.00318	0.927	1.0033	0.07618	0.00012
26	0.98525	0.907	0.9853	0.07825	0.00005
27	1.01445	0.9395	1.0146	0.07495	0.00015
28	1.00779	0.9398	1.0148	0.06799	0.00701
29	0.99442	0.9176	0.9946	0.07682	0.00018
30	0.98284	0.9051	0.983	0.07774	0.00016
MSE				0.00553	0.0000068
No.	6	12	7		
of					
iter.					



Figure4.Comparison between actual and estimated values of the bus voltage magnitude

Bus	Angle	Angle	Angle	Abs.	Abs.
No.	Actual	WLS	Proposed	Error	Error
	(rad.)	(rad.)	Algorithm	WLS	Proposed
			(rad.)		Algorithm
1	0	0	0	0	0
2	-0.09345	-0.1093	-0.0941	0.01585	0.00065
3	-0.13144	-0.1543	-0.1329	0.02286	0.00146
4	-0.16204	-0.1903	-0.1636	0.02826	0.00156
5	-0.24738	-0.2879	-0.2477	0.04052	0.00032
6	-0.193	-0.2269	-0.1951	0.0339	0.0021
7	-0.22453	-0.2626	-0.2258	0.03807	0.00127
8	-0.20629	-0.2437	-0.2096	0.03741	0.00331
9	-0.24547	-0.2877	-0.2472	0.04223	0.00173
10	-0.2735	-0.3202	-0.275	0.0467	0.0015
11	-0.24547	-0.2877	-0.2472	0.04223	0.00173
12	-0.26397	-0.3088	-0.2643	0.04483	0.00033
13	-0.26397	-0.3088	-0.2643	0.04483	0.00033
14	-0.27928	-0.3266	-0.2797	0.04732	0.00042
15	-0.2794	-0.3269	-0.2801	0.0475	0.0007
16	-0.27271	-0.319	-0.2737	0.04629	0.00099
17	-0.27696	-0.3241	-0.2784	0.04714	0.00144
18	-0.28984	-0.3389	-0.2906	0.04906	0.00076
19	-0.29262	-0.3422	-0.2936	0.04958	0.00098
20	-0.28886	-0.3379	-0.2899	0.04904	0.00104
21	-0.28305	-0.3313	-0.2845	0.04825	0.00145
22	-0.27892	-0.3266	-0.2804	0.04768	0.00148
23	-0.28326	-0.3315	-0.2847	0.04824	0.00144
24	-0.2845	-0.333	-0.2857	0.0485	0.0012
25	-0.28051	-0.3277	-0.2807	0.04719	0.00019
26	-0.28805	-0.3361	-0.2882	0.04805	0.00015
27	-0.27325	-0.3193	-0.2734	0.04605	0.00015
28	-0.20449	-0.2407	-0.207	0.03621	0.00251
29	-0.29509	-0.3449	-0.2952	0.04981	0.00011
30	-0.31079	-0.3633	-0.3109	0.05251	0.00011
MSE				0.00185	0.0000017

Table 5.Actual voltage angles, estimated angles, and errors for the 30 Bus system





Table 6. Comparison of the estimation accuracy in bus voltage magnitude					
	E) in bus voltage magnitude				
Test System	WLS in Polar Form	Proposed Algorithm			
IEEE-14 bus test	0.00311	0.000005			
System					
IEEE-30 bus test	0.00553	0.0000068			
System					

- I- I - C	<b>C</b>	- 6 - 1		• •	lesses such that a	
able 6.	Comparison	of the	estimation	accuracy in	i bus voitag	e magnitude

Track Constant	Mean Square Error (MSE) in bus phase angle	
Test System	WLS in Polar Form	Proposed Algorithm
IEEE-14 bus test	0.000655	0.00000004
System		
IEEE-30 bus test	0.00185	0.0000017
System		

Table 8.	Execution	time in	seconds
Tuble 0.	EXecution	thine in	Jeconas

Test System	CPU time in (Sec.)	
	WLS in Polar Form	Proposed Algorithm
IEEE-14 bus test	0.039422	0.021803
System		
IEEE-30 bus test	0.15386	0.063552
System		

#### 6. Conclusions

An algorithm to obtain the optimal estimate of the state vector has been presented. The formulation of estimator model was based on rectangular coordinates of the state variables. A predictor-corrector technique has been used for solving the nonlinear model of the estimator. The proposed algorithm was enriched by placing the PMU meters optimally. The applications of the proposed algorithm on test systems are given in the paper. The results obtained reveal the superiority of the developed algorithm compared to the conventional algorithm in terms of the execution time, accuracy and the number of iterations for the system to be converged. The proposed algorithm is very promising for real time monitoring application.

### 7. Abbreviations

SCADA	Supervisory Control and Data Acquisition
PSO	Particle Swarm Optimization
WLS	Weighted Least Square
PMUs	Phasor Measurement Units
GA	Genetic Algorithm
SE	State Estimation
AI	Artificial Intelligence
FF	Fitness Function

IEEE	Institute of Electrical and Electronic Engineers
MSE	Mean Square Error
WLAV	Weighted Least Absolute Value
LMS	Least Median of Squares

### Acknowledgement

The authors would like to thank Mustansiriyah University <u>www.uomustansiriyah.edu.iq</u> <u>Baghdad-Iraq</u> for its support and providing the facilities to carry out the present work.

# 8. References

- 1. Schweppe, F.C. and Wildes, J.(1970). "Power system static state estimation", Part I:Exact model. IEEE Trans. Power. Appar. Syst., Vol. PAS-89, pp.120-125.
- 2. Schweppe, F.C. and Wildes, J.(1970). "Power system static state estimation", Part I:Approximate model. IEEE Trans. Power. Appar. Syst., Vol. PAS-89, pp.125-130.
- 3. Praise, M. and Bose, A.(1988). "A topology processor that tracks network modifications over time", IEEE Trans. Power. Systems., Vol. 3, No. 3, pp.992-998.
- 4. Simoes Costa, A. and Leao, J.A. (1993). "*Identification of topology errors in state estimation*", IEEE Trans. Power. Systems., Vol. 8, No. 4, pp.1531-1538.
- 5. Singh, H. and Alvarado, F.L. (1995). "Network topology determination using least absolute value state estimation", IEEE Trans. Power. Systems, Vol. 10, No. 3, pp.1159-1165.
- 6. Vinod Kumar, D.M., Srivastava, S.C., Shah,S. and Mathur,S. (1996). "*Topology processing and static state estimation using artificial neural networks*", IEEE Proceeding on Generation, Transmission & Distribution, Vol. 143, No. 1, pp.99-105.
- Souza, J.C.S., Leite da Silva, A.M., and Alves de Silva, A.P. (1998). "Online topology determination and bad data suppression in power system operation using artificial neural networks", IEEE Trans. Power. Systems., Vol. 13, No. 3, pp.796-803.
- 8. Farrokhabadi, M. and Vanfretti, L. (2014). "An Efficient automated topology processor for state estimation of power transmission networks", Electric Power Systems Research, Vol. 106, pp.188-202.
- 9. Da Silva, N.S., Simoes Costa, A., Clements, K.A. and Andreoli, E. (2016). "Simultaneous estimation of state variables and network topology for power system real time modeling", Electric Power Systems Research, Vol. 133, pp.338-346.
- Cho, Y-S. (2017). "A novel approach to enhance the accuracy of network topology optimization", Electric Power Components and Systems, Vol. 45, No.2, pp.131-146.
- 11. Bargiela, A., Irving, M.R., and Sterling, M.J.H. (1986). "Observability determination in power system state estimation using a network flow technique", IEEE Trans. Power. Systems., Vol. 4, No. 2, pp.108-112.

- 12. Christensen, G.S., Soliman, S.A. and Rouhi, A.H. (1989). "An observability algorithm for sequential measurement processing in power system state estimation", Electric Power Components and Systems, Vol. 17,No.3, pp.203-219.
- 13. Gou,B. (2007). "Observability analysis for state estimation using Hachtel's augmented matrix method", Electric Power Systems Research, Vol. 77, No. 7, pp.865-875.
- Pruneda, R.E., Solares, C., Conejo, A.J. and Castillo, E. (2010). "An Efficient algebraic approach to observability analysis in state estimation", Electric Power Systems Research, Vol. 180, No.3, pp.277-286.
- Koglin, H.J, Neisius, TH., Beibler, G. and Schmitt, K.D. (1990). "Bad data detection and identification", Inter. Journal of Electric Power & Energy Systems, Vol. 4, No.1, pp.94-103.
- Salehfar, H. and Zhao, R. (1995). " A neural network pre estimation filter for bad data detection and identification in power system state estimation", Electric Power Systems Research, Vol. 34, No.2, pp.127-134.
- 17. Chen, J. and Abur, A. (2006). "Placement of PMUs to enable bad data detection in state estimation", IEEE Trans. Power. Systems., Vol. 21, No. 4, pp.1608-1615.
- Korres, G.N. and Manousakis N.M. (2011). "State estimation and bad data processing for systems including PMU & SCADA measurements", Electric Power Systems Research, Vol. 81, No.7, pp.1514-1524.
- Gou, B. and Kavasseri, R.G. (2014). "Unified PMU placement for observability and bad data detection in state estimation", IEEE Trans. Power. Systems., Vol. 29, No. 6, pp.2573-2580.
- Singh, H. and Alvarado, F.L. (1994). "Weighted least absolute value state estimation using interior point methods", IEEE Trans. Power. Systems., Vol. 9, No. 3, pp.1478-1484.
- Madtharad, C., Premrudeepreechacharn, S. and Watson N.R. (2003). "Power system state estimation using singular value decomposition", Electric Power Systems Research, Vol. 67, pp.99-107.
- Gomez-Exposit, E., Gomez-Qniles, C. and de laVilla Jean, A. (2012). "Bilinear power system state estimation", IEEE Trans. Power. Systems., Vol. 27, No. 1, pp.493-501.
- 23. Chen, Y., Ma, J., Lin, F. and Mei S. (2015). "*A bilinear robust state estimator*", Inter. Journal on Electrical Energy Systems, Vol. 6, pp.123-144.
- 24. Aravindhababu, P. and Neela, R. (2008). "A reliable & fast decoupled weighted least square state estimation for power systems", Electric Power Components and Systems, Vol. 36, pp.1200-1207.
- Abbassi, A.R. and Seifi A.R. (2013). "A new coordinated approach to state estimation in integrated power systems", Electric Power & Energy Systems, Vol. 45, pp.152-158.
- Jiang, X-T., Chow, J.H., Fardanesh,B.,Maragal,D.,Stefopoulos,G. and Razanousky,M. (2015). "Power system state estimation using a direct non-iterative method", Electric Power & Energy Systems, Vol. 73, pp.361-368.

- Aien, M., Rashidinegad, M., Kouhi, S., Fatuhifiruzabad, M. and Ravadanegh, S.N.. (2014). "*Real time probabilistic power system state estimating*", Electric Power & Energy Systems, Vol. 62, pp.383-390.
- Mallik, S.K., Chakrabarti,S. and Singh, S.N. (2014). "A robust regularized hybrid state estimator for power systems", Electric Power Components and Systems, Vol. 42,No.7, pp.671-681
- 29. Baldwin, T., Mili, L., Boisen Jr, M and Adapa, R. (1993). "Power system observability with minimal phasor measurements placement", IEEE Trans. Power. Systems., Vol. 8, No. 2, pp.707-715.
- Rakpenthai, C. Premrudeepreechacham S. Uatrongjit, S. and Watson, N. (2007).
   "An optimal PMU placement method against measurement loss and branch outage", IEEE Trans. Power.Delivery., Vol. 22, No. 1, pp.101-107.
- Abbasy, N. and Ismail, H. (2009). "A unified approach for the optimal PMU location for power state estimation", IEEE Trans. Power. Systems., Vol. 24, No. 2, pp.806-813.
- 32. Abur, A. and Gomez Exposito, A. (2004). "Power System State Estimation, Theory and Implementation", Marcel Dekker, Inc, USA.
- 33. Kusic, G.L. (2003). "Coomputer-Aided Power systems Analysis ", second printing, Prentice-Hill of India, India.
- 34. Kennedy, J. and Eberhart, R. (1995). "*Particle swarm optimization In:*", Proceeding of the 1995 IEEE 1<sup>st</sup> conference on neural networks, Vol.4, pp.1942-1948.
- Al-Anbarri, K. (2017). "A Novel load flow solution based on a predictor- corrector technique", Proceeding of the 1st International Conference on Recent Trends of Engineering Sciences and Sustainability, Baghdad, pp.327-331.
- 36. <u>Https://www.mathworks.com/MATLABcentral/</u> file exchange.
- Soheili, A.R., Ahmadian, S.A. and Naghipoor, J. (2008). "A family of predictorcorrector methods based on weight combination of quadratures for solving nonlinear equations", International Journal of Nonlinear Science, vol. 6, No.1, pp. 29-33.
- Hafiz, M.A.and Bahgat, M.S.M. (2012). "An efficient two-step iterative method for solving system of nonlinear equations", Journal of Mathematics Research, vol. 4, No.4, pp. 28-34.

#### Appendix A

iterations as compared with the traditional numerical methods. For the following nonlinear algebraic equation:

$$\mathbf{F}(\mathbf{x}) = \mathbf{0} \tag{A.1}$$

Assuming that x be the simple zero of this equation. Equation (A.1) can be written as[37,38]:

$$(x) = F(x_i) + \int_{x_i}^{x} F'(t)dt$$
A.2

The second term of equation (A.2) involves multiple integrals and can be approximated with average of midpoint and Simpson quadrature formulas, then we have:

$$\int_{x_i}^{x} F'(t)dt = \frac{x - x_i}{2} F'\left(\frac{x_i + x}{2}\right) + \frac{x - x_i}{12} \left[F'(x_i) + 4F'\left(\frac{x_i + x}{2}\right) + F'(x)\right]$$
A.3

Substituting (A.3) into (A.2) we have:

$$F(x) = F(x_i) + \frac{x - x_i}{2} F'\left(\frac{x_i + x}{2}\right) + \frac{x - x_i}{12} [F'(x_i) + 4F'\left(\frac{x_i + x}{2}\right) + F'(x)$$
A.4

Since, F(x) = 0 then

$$[x] = [x_i] + 12[G_{(x_i)} + 10G_{(w_i)} + G_{(y_i)}]^{-1}[F(x_i)]$$
A.5

$$[w_{i}] = \begin{bmatrix} w_{1} \\ w_{2} \\ \vdots \\ w_{n} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} y_{1} + x_{1} \\ y_{2} + x_{2} \\ \vdots \\ y_{n} + x_{n} \end{bmatrix}, [x_{i}] = \begin{bmatrix} x_{1} \\ x_{2} \\ \vdots \\ x_{n} \end{bmatrix}, [y_{i}] = \begin{bmatrix} y_{1} \\ y_{2} \\ \vdots \\ y_{n} \end{bmatrix}$$
A.6

It is an implicit way since  $[x_{i+1}]$  occurs on both sides of the equation. To carry out this implicit way, one has to calculate the approximate solution implicitly, which is itself a difficult problem. To overcome this defect, the prediction and correction method is typically used. By using formula (A.6), a two-step iterative method for solving the system of nonlinear equation (A.1) can be obtained. For a given  $x_0$ , the approximate solution [ $x_{i+1}$ ] is calculated by iterative scheme as follows:

$$y_i = x_i - \frac{F(x_i)}{F'(x_i)}$$
A.7

$$x_{i+1} = x_i - \frac{12 F(x_i)}{F'(x_i) + 10F'(\frac{x_i + y_i}{2}) + F'(y_i)}$$
 A.8

In a compact form, equation A.9 can be written as:

$$[x_{i+1}] = [x_i] + 12[G_{(x_i)} + 10G_{(w_i)} + G_{(y_i)}]^{-1}[F(x_i)]$$
A.9